Technical Note

Microfluidic Method for Synthesizing Cu₂O Nanofluids

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I. Introduction

ANOFLUIDS, fluid suspensions of nanometer-sized particles, have recently been demonstrated to have thermal conductivities far superior to that of the liquid alone [1–4]. This and their other distinctive features offer unprecedented potential for many applications in various fields, including energy, biological, pharmaceutical, chemical, electronic, environmental, material, medical, and thermal engineering industries [1–8]. Yet the functional outcomes of existing nanofluids have not been satisfactory because of the inadequacies of conventional synthesis approaches in engineering microstructures and properties of nanofluids [1–9].

For creating nanofluids by design, we have recently developed a one-step chemical solution method (CSM) that is capable of synthesizing nanofluids of various microstructures [9–11]. The method has been successfully applied to produce the nine kinds of nanofluids [9–11]. The nanofluids synthesized by the CSM have both higher conductivity enhancement and better stability than those produced by other methods. The CSM is also distinguished from the others by its controllability. The nanofluid microstructure can be easily varied and manipulated by adjusting synthesis parameters such as temperature, acidity (pH), ultrasonic and microwave irradiation, types and concentrations of reactants and additives, and the order in which the additives are added to the solution [9–11].

Problems with the CSM come from that reactions take place in macroscale batch reactors such as beakers and flasks. The CSM uses a bottom-up approach to generate nanoparticles through chemical reactions in the liquid phase, and thereby it has the potential to manipulate atoms and molecules for synthesis of tailor-made nanofluids. However, the difficulty of controlling the microscale while operating at the macroscale is insuperable. Mixing in a macroscale batch reactor is usually achieved by stirring. In this case, the fluid entity is broken into fragments by circular motion. The last part of mixing takes place based on molecular diffusion. In the diffusion process, the mixing time t depends on the diffusion path din the form of $t \propto d^2/D$, where D is the diffusion coefficient. Therefore, if the diffusion path becomes smaller, the mixing time becomes shorter. However, it is very difficult to make small-sized fragments by conventional stirring in solution phase. At the macroscale, therefore, mixing time is usually much larger than reaction time. The reaction rate is normally determined by the mixing time and is usually very low. Moreover, the longer mixing time and lack of effective ways to accurately control mixing also lead to poor product selectivity of competitive parallel reactions and competitive

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consecutive reactions, thereby yielding poor quality of synthesized nanofluids containing some undesired side products. Because of the work-up demand, a batch-model operation is not commercially economical. The repeatability of nanofluids' structures is also poor with the batch-model operation.

To resolve these critical issues, we propose to replace batch-based macroreactors in the CSM by continuous-flow microfluidic microreactors, allowing a continuous and scalable (simply by numbering-up) synthesis of nanofluids with a more accurate and effective control over particle microstructures such as the size, distribution, and shape. Here, we report such a microfluidic system for synthesizing Cu_2O nanofluids: suspensions of Cu_2O nanoparticles in water.

II. Synthesis

Synthesizing the Cu_2O nanofluids by the CSM is based on following chemical reactions, in order [11]:

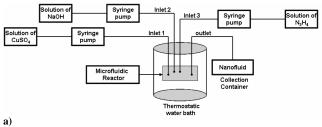
$$Cu SO4 + 2NaOH = Cu(OH)2 + Na2SO4$$
 (1)

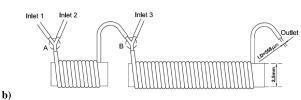
$$Cu(OH)_2 \stackrel{\triangle}{=} CuO + H_2O$$
 (2)

$$4CuO + N_2H_4 = 2Cu_2O + N_2 + 2H_2O$$
 (3)

The reaction between cupric-sulfate (CuSO₄) and sodium-hydrate (NaOH) yields cupric-hydroxide (Cu(OH)₂) and sodium sulfate (Na₂SO₄) [Eq. (1)]. The cupric-hydroxide Cu(OH)₂ will quickly decomposed into cupric-oxide (CuO) and water (H₂O) under some heating [Eq. (2)]. The cupric-oxide (CuO) is then reduced into cuprous-oxide (Cu₂O) with the hydrazine-hydrate (N₂H₄) as the reducer and nitrogen (N₂) and water (H₂O) as the byproducts [Eq. (3)].

Figure 1a shows the microfluidic system in which these chemical reactions take place. The CuSO₄ and NaOH fluids are pumped by





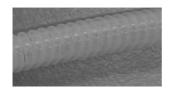
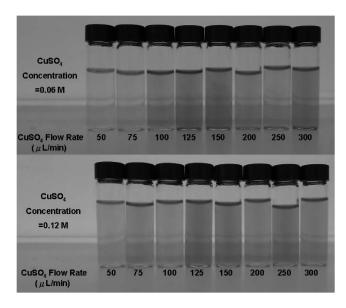
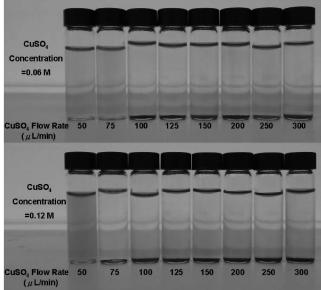


Fig. 1 Microfluidic one-step chemical solution method for Cu₂O nanofluids synthesis: a) test setup, b) microfluidic reactor, and c) PTFE microbore tubing coil.





a) 24-hour standing

b) 100-hour standing

Fig. 2 Cu₂O nanofluids synthesized at different CuSO₄ molar concentrations and flow rates: a) after 24 h standing; b) after 100 h standing.

high-precision syringe pumps (Cole-Parmer Instrument Company) and forced to flow through the microfluidic reactor (Fig. 1b) that is immersed in a thermostatic water bath with a fixed temperature $40^{\circ}C$ (IKA RCT Basic and EDS-D5). As they travel from point A to point B and receive heat from the water bath, the chemical reactions (1) and (2) take place. The N_2H_4 fluid is injected into the microfluidic reactor from inlet 3 (Fig. 1b) also by the high-precision syringe pump (Cole-Parmer Instrument Company); and the chemical reaction (3) takes place as the fluid streams travel further in the microfluidic reactor towards its outlet (Fig. 1b). The output channels of the

microfluidic reactor allow the nanofluids to vent to the collecting container at atmosphere pressure.

By this method, we can continuously synthesize Cu_2O nanofluids whose microstructures can be varied by adjusting synthesis parameters such as reactant concentrations, flow rates of reactant fluids and geometry of microfluidic reactor. All the chemicals used in our experiments are with a nominal purity higher than 99% and used as received (Taikangda, Ltd.). The water is prepared in our laboratory by double distillation. NaOH solution is prepared to have a fixed pH value 12. The N_2H_4 concentration is fixed at 0.3 M. To enhance the

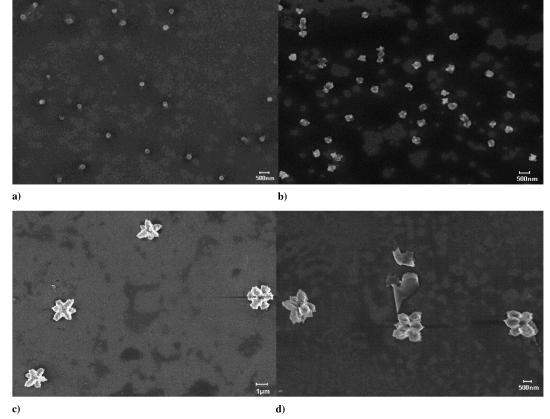


Fig. 3 SEM images of some Cu_2O particles showing $CuSO_4$ concentrations and $CuSO_4$ flow rates, respectively, of a) 0.12 M and 300 $\mu L/min$, b) 0.06 M and 75 $\mu L/min$, c) 0.06 M and 100 $\mu L/min$, and d) 0.06 M and 250 $\mu L/min$.

		${ m CuSO_4}$ flow rate, $\mu{ m L/min}$							
CuSO ₄ concentration	50	75	100	125	150	200	250	300	
0.06 M 0.12 M	103.4 271.6	81.7 374.9	116.0 194.1	131.1 147.9	84.3 176.2	154.3 211.6	129.7 329.8	199.2 197.8	

Table 1 Variations of particle average diameter (nm) with the CuSO₄ concentration and flow rate

nanofluid stability and prevent the particle aggregation, 5 g/L polyvinyl pyrrolidone (PVP, a chemical surfactant) is premixed with CuSO₄ solution. We fix the CuSO₄ molar concentration at 0.06 and 0.12 M, respectively, to investigate its effect on the nanofluids microstructure and thermal conductivity. For each of two CuSO₄ concentration values, we examine the effect of fluid flow rates by setting the CuSO₄ flow rate at 50, 75, 100, 125, 150, 200, 250, and 300 μ L/ min, respectively, and keeping the flow rate ratio of CuSO₄, NaOH, and N₂H₄ fluids as 1:1:2. The flow rates are controlled and measured by the syringe pumps.

The microfluidic reactor consists of 4-m-long polytetrafluoro-ethylene (PTFE) microbore tubing coil with an inner diameter of 558 μ m (Cole-Parmer Instrument Company), which winds tightly on a cylinder of 2.5 mm in diameter (Figs. 1b and 1c). The two parts of the coil are connected by a Y-type connector (Cole-Parmer Instrument Company); and their lengths are 1 and 3 m, respectively. Both are long enough to ensure the completion of reactions (1) and (2) in the first part and reaction (3) in the second part, respectively. This microfluidic reactor can have a very rapid mixing between reactant fluids due to both the short diffusion length and the centrifugal-force-driven transverse secondary flow in curved channels [12–15].

III. Results and Discussion

Figure 2 shows the synthesized nanofluids with different values of CuSO₄ molar concentration and eight sets of fluid flow rates after 24 and 100 h standing, respectively. The fluid is very stable, and no bulk phase separation has been observed for all samples 24 h after its preparation (Fig. 2a). The nanofluids synthesized at the CuSO₄ flow rate of 50 and 75 μ L/ min are still stable even after 100 h standing (Fig. 2b). This is especially important considering that the PVP concentration used is only one-third of that in [11] and it is typically rare to maintain nanofluids synthesized by conventional approaches in a homogeneous stable state for more than 24 h [2].

Figure 3 typifies the SEM (scanning electron microscope) images of nanoparticles (Hitachi S-4800 FEG SEM, Japan), showing that the particles can be changed from a spherical shape to a polyhedral, starfishlike, and even flowerlike one by varying the $CuSO_4$ con-

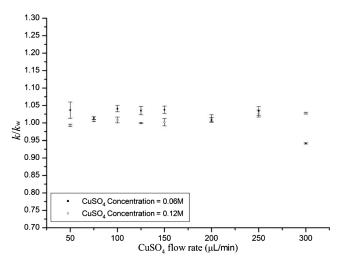


Fig. 4 Variation of k/k_w with CuSO₄ molar concentration and flow rate (k is nanofluid thermal conductivity, and k_w is water thermal conductivity).

centration and/or fluid flow rates. Variations of particle average diameter with the CuSO_4 concentration and flow rate are measured by dynamic light-scattering system (Delsa Nano C, Beckman Coulter) and are shown in Table 1.

Figure 4 shows the variation of conductivity ratio k/k_w with the ${\rm CuSO_4}$ concentration and flow rate at the room temperature. Here, k and k_w are the thermal conductivity of the nanofluid and the water, respectively, measured by the standard transient line heat source method (KD2 Pro; Decagon Devices, Inc.) [16]. For each data point in Fig. 4, an average value over three readings is used. The error bar indicates the standard deviation calculated based on the procedure described in [17]. A variation of k/k_w from 0.94 to 1.04 is observed. Therefore, the presence of nanoparticles can either enhance or weaken fluid heat conduction, a phenomenon predicted by the thermal-wave theory [9,18,19]. Although the ${\rm CuSO_4}$ concentration and flow rate can change the shape of nanoparticles significantly (Fig. 3), they vary the conductivity ratio k/k_w only moderately (Fig. 4). Therefore, the conductivity enhancement is insensitive to the particle shape for this type of nanofluids.

IV. Conclusions

Conventional nanofluid synthesis approaches have not been satisfactory because of their inadequacies in engineering microstructures of nanofluids. The recently developed one-step chemical solution method (CSM) takes advantage of the ability of manipulating atoms and molecules through chemical reactions in the liquid phase. However, the difficulty of controlling the microscale while operating at the macroscale is insuperable. By replacing batch-based macroreactors in the CSM by continuous-flow microfluidic microreactors, a novel microfluidic one-step CSM is developed for effective synthesis of nanofluids with controllable microstructures. The technique has been successfully applied to synthesize Cu₂O nanofluids with spherical, polyhedral, starfishlike, and flowerlike nanoparticles. The Cu₂O nanofluids synthesized by this method have better stability than those produced by other methods and are with a conductivity enhancement insensitive to the particle shape.

Acknowledgment

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References

- Choi, S. U. S., Zhang, Z. G., and Keblinski, P., "Nanofluids," *Encyclopedia of Nanoscience and Nanotechnology*, H. S. Nalwa, ed., American Scientific, New York, 2004, pp. 757–773.
- [2] Peterson, G. P., and Li, C. H., "Heat and Mass Transfer in Fluids with Nanoparticle Suspensions," *Advances in Heat Transfer*, Vol. 39, 2006, pp. 257–376. doi:10.1016/S0065-2717(06)39003-X
- [3] Das, S. K., Choi, S. U. S., Yu, W. H., and Pradeep, T., Nanofluids: Science and Technology, Wiley, Hoboken, NJ, 2008.
- [4] Wu, D. X., Zhu, H. T., Wang, L. Q., and Liu, L. M., "Critical Issues in Nanofluids Preparation, Characterization and Thermal Conductivity," *Current Nanoscience*, Vol. 5, 2009, pp. 103–112. doi:10.2174/157341309787314548
- [5] Choi, S. U. S., "Nanofluids: From Vision to Reality Through Research," *Journal of Heat Transfer*, Vol. 131, 2009, pp. 033106/1–033106/9. doi:10.1115/1.3056479
- [6] Eastman, J. A., Phillpot, S. R., Choi, S. U. S., and Keblinski, P., "Thermal Transport in Nanofluids," *Annual Review of Materials Research*, Vol. 34, 2004, pp. 219–246. doi:10.1146/annurev.matsci.34.052803.090621

- [7] Phelan, P. E., Bhattacharya, P., and Prasher, R. S., "Nanofluids for Heat Transfer Applications," *Annual Review of Heat Transfer*, Vol. 14, 2005, pp. 255–275.
- [8] Sobhan, C. B., and Peterson, G. P., Microscale and Nanoscale Heat Transfer: Fundamentals and Engineering Applications, CRC Press, Boca Raton, FL, 2008.
- [9] Wang, L. Q., and Wei, X. H., "Nanofluids: Synthesis, Heat Conduction, and Extension," *Journal of Heat Transfer*, Vol. 131, 2009, Paper 033102. doi:10.1115/1.3056597
- [10] Wei, X. H., Zhu, H. T., and Wang, L. Q., "CePO₄ Nanofluids: Synthesis and Thermal Conductivity," *Journal of Thermophysics and Heat Transfer*, Vol. 23, 2009, pp. 219–222. doi:10.2514/1.38778
- [11] Wei, X. H., Zhu, H. T., Kong, T. T., and Wang, L. Q., "Synthesis and Thermal Conductivity of Cu₂O Nanofluids," *International Journal of Heat and Mass Transfer*, Vol. 52, 2009, pp. 4371–4374. doi:10.1016/j.ijheatmasstransfer.2009.03.073
- [12] Wang, L. Q., and Liu, F., "Forced Convection in Slightly Curved Microchannels," *International Journal of Heat and Mass Transfer*, Vol. 50, 2007, pp. 881–896. doi:10.1016/j.ijheatmasstransfer.2006.08.016
- [13] Wang, L. Q., and Yang, T. L., "Multiplicity and Stability of Convection in Curved Ducts: Review and Progress," *Advances in Heat Transfer*, Vol. 38, 2004, pp. 203–255. doi:10.1016/S0065-2717(04)38004-4

- [14] Wang, L. Q., and Cheng, K. C., "Flow Transitions and Combined Free and Forced Convective Heat Transfer in Rotating Curved Channels: The Case of Positive Rotation," *Physics of Fluids*, Vol. 8, 1996, pp. 1553–1573. doi:10.1063/1.868930
- [15] Liu, F., and Wang, L. Q., "Analysis on Multiplicity and Stability of Convective Heat Transfer in Tightly Curved Rectangular Ducts," *International Journal of Heat and Mass Transfer*, Vol. 52, 2009, pp. 5849–5866. doi:10.1016/j.ijheatmasstransfer.2009.07.019
- [16] Tavman, S., and Tavman, I. H., "Measurement of Effective Thermal Conductivity of Wheat as a Function of Moisture Content," *International Communications in Heat and Mass Transfer*, Vol. 25, 1998, pp. 733–741. doi:10.1016/S0735-1933(98)00060-8
- [17] Buongiorno, J., Venerus, D. C., Prabhat, N., McKrell, T., Townsend, J., and Christianson, R., et al., "A Benchmark Study on the Thermal Conductivity of Nanofluids," *Journal of Applied Physics*, Vol. 106, 2009, Paper 094312. doi:10.1063/1.3245330
- [18] Wang, L. Q., Zhou, X. S., and Wei, X. H., Heat Conduction: Mathematical Models and Analytical Solutions, Springer-Verlag, Heidelberg, Germany, 2008.
- [19] Wang, L. Q., Xu, M. T., and Wei, X. H., "Multiscale Theorems," Advances in Chemical Engineering, Vol. 34, 2008, pp. 175–468. doi:10.1016/S0065-2377(08)00004-5